

# Hydrology and Hydraulic Study For

## Prepared For:

Imperial Beach Resort, LLC  
10450 South Eastern Ave., Suite 100  
Henderson, NV 89052  
APN No. 625-380-27-00

## Prepared By:

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## Job Number:

149346

## Prepared:

December 14, 2015

## Revised:

February 16, 2017

**Michael Baker**

INTERNATIONAL

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## Section 1 Project Description and Scope

### 1.1. Project Data

**Project Owner:** Imperial Beach Resort, LLC  
10450 S. Eastern Ave., Suite #100  
Henderson, NV 89052  
Kenneth Knudsen

Project Site Address: 1060 Seacoast Dr., Imperial Beach, CA

APN Number(s): 625-380-27-00

Project Location: Latitude: 32.577025  
Longitude: -117.132070

Project Site Area: 1.00 Acres

**Adjacent Streets:**

North: Ebony Avenue  
South: Imperial Beach Boulevard  
East: Seacoast Drive  
West: None

**Adjacent Land Uses:**

North: Residential  
South: Residential  
East: Residential/Commercial  
West: Public Beach

### 1.2. Scope of Report

This report addresses the Hydrologic and Hydraulic aspects of the project. This report does not discuss required water quality measures to be implemented on a permanent basis, nor does it address construction storm water issues. Post construction storm water issue discussions can be found under separate cover in the project "Storm Water Quality Management Plan".

## 1.3. Project Site Information

### 1.3.1 Project Location

The project is located in beautiful Imperial Beach, California. The project is located in the southwesterly portion of the City and is adjacent to the beach and Pacific Ocean. Please refer to Figure 1 below for a Vicinity Map.

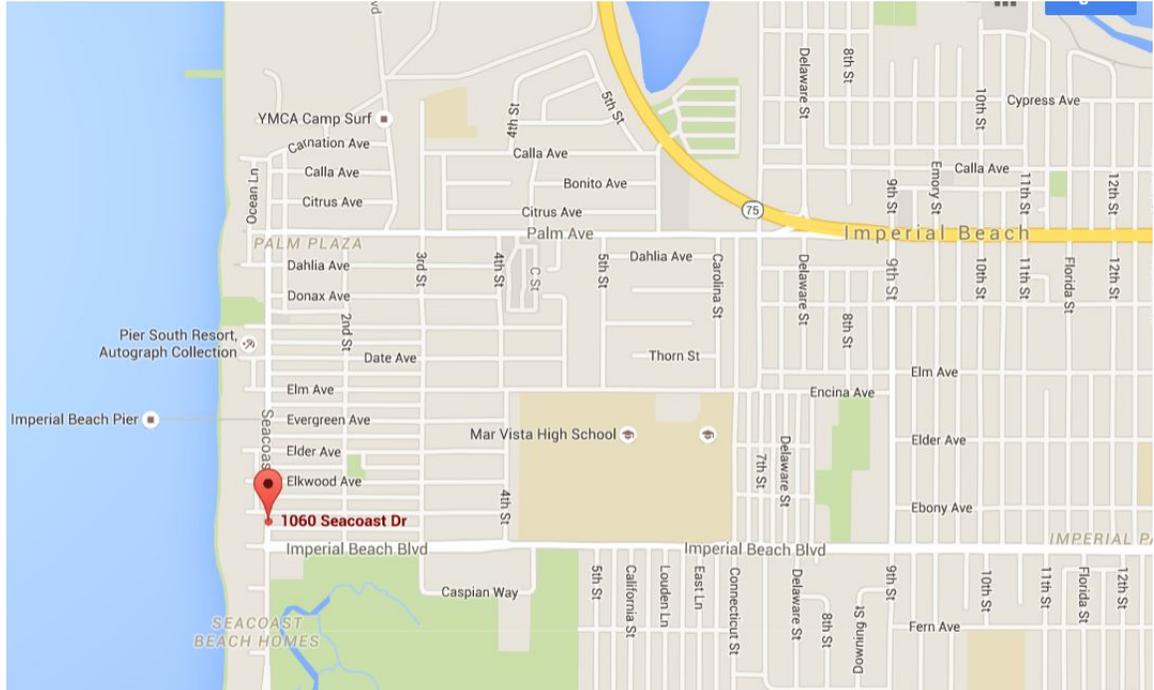


Figure 1: Vicinity Map

### 1.3.2 Project Description

The project proposes the construction of a 100 room hotel with underground parking. The project also proposes new underground utility services and access drives for the underground parking.

### 1.3.3 Site Topography

The project area is currently fully developed, and is home to multiple commercial buildings. Drainage from the site is broken down into 2 basins. Basin 1 encompasses the western half of the site, with runoff surface flowing southwest onto Imperial Beach Drive. Basin 2 encompasses the eastern half of the site with flows drainage towards Seacoast Drive. The site is flat with all slopes under 5%.

### 1.3.4 Land Use and Vegetation

The site has been partially graded for the preparation for the proposed project. There is no significant vegetation on site, and no native vegetation.

### 1.3.5 FEMA Information

The Federal Emergency Management Agency (FEMA) has mapped the floodplain site. The project does not lie within any mapped floodplain (FIRM Panel 0673C2134G). The project lies within Zone X Unshaded which is outside the 500-year floodplain.

#### a) Flood Zone Definitions

Zone A -- Areas subject to inundation by the 1-percent-annual-chance flood event generally determined using approximate methodologies. Because detailed hydraulic analyses have not been performed, no Base Flood Elevations (BFEs) or flood depths are shown. Mandatory flood insurance purchase requirements and floodplain management standards apply.

Zone AE -- Areas subject to inundation by the 1-percent-annual-chance flood event determined by detailed methods. Base Flood Elevations (BFEs) are shown. Mandatory flood insurance purchase requirements and floodplain management standards apply.

Zone X (Shaded) – Areas between the limits of the base flood and the 0.2-percent-annual-chance (or 500-year) flood.

Zone X (Unshaded) Areas of minimal flood hazard, which are the areas outside the SFHA and higher than the elevation of the 0.2-percent-annual-chance flood.

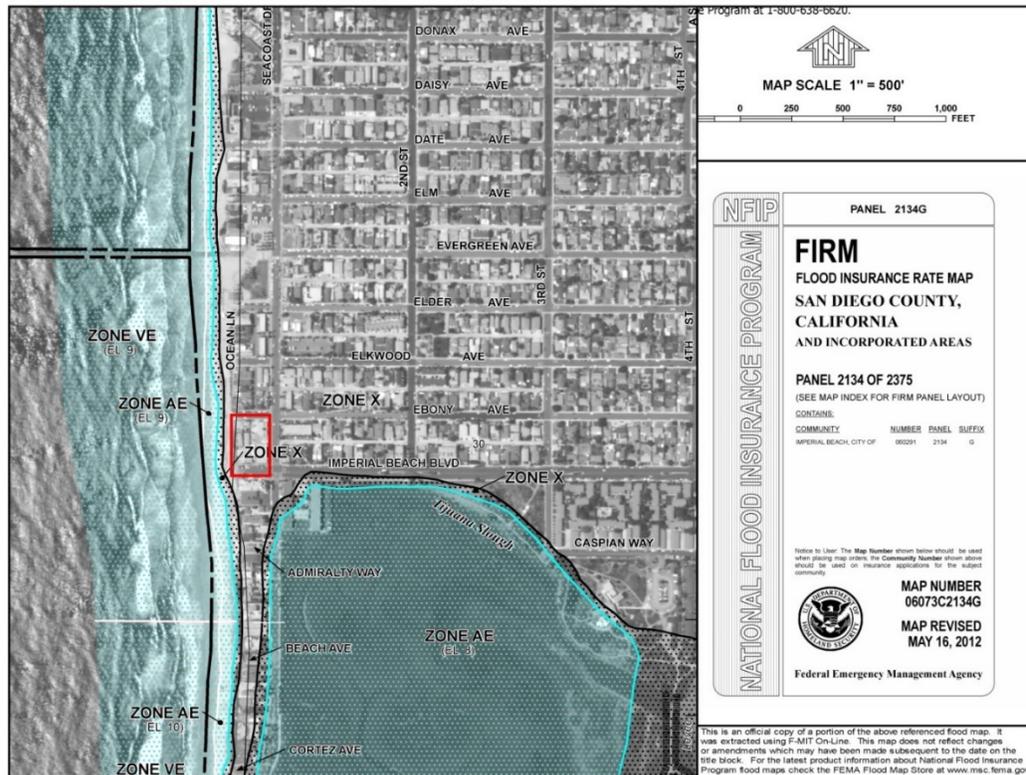


Figure 2: FEMA Firmette

### 1.3.6 Existing Drainage Improvements

There are no formal drainage improvements on site in the existing condition or the pre-demolition condition. Drainage from the project surface flows in all directions to the surrounding streets and beach.

### 1.3.7 Proposed Improvements

In the proposed condition, drainage will be collected in a series of catch basins and roof drains. Drainage will be routed to the parking garage where the flows will enter a storage tank capable of handling the 85<sup>th</sup> percentile rainfall. The flows from the storage tank will gravity flow through a modular wetland system (Proprietary Biofiltration Unit, BF-3), before flowing to a wet well. Flows are then pumped from the wet well to a curb pipe at the northwest corner of the site on Ebony Avenue. From this discharge point treated storm water comingles with street drainage before flowing westerly within the gutter and discharging to the beach via gutter. The pump system is being designed by a separate contractor. Drainage from the public sidewalks and surrounding public hardscape will continue to flow into the adjacent streets and flow untreated into the gutter before being discharged to the Pacific Ocean, as in the existing condition.

## Section 2 Study Objectives

The specific objectives of this study are as follows:

- To provide hydrologic analysis of the project site for the 100-year, 6-hour storm event under existing and proposed conditions,
- To ensure that no additional runoff or downstream impacts occur due to this project.

## Section 3 Methodology

### 3.1. Hydrology

Because the size of the site, the Rational Method was chosen for the analysis. The rational method is used for situations where the basin is less than 1 square mile, and the flow path for the drainage does not exceed 500 feet. Therefore the hydrologic analysis has been completed using the Rational Method ( $Q = CIA$ ) (see County of San Diego Hydrology Manual, Section 3). Whereas,

**Q** = rate of flow in cubic feet per second

**C** = Coefficient of runoff,

**I** = intensity of rainfall based on the time of concentration and the 6-hour, 100-year precipitation

**A**=Area of the basin.

Runoff coefficients were obtained using Table 3-1 of the County of San Diego Hydrology Manual. A value of 0.85 was chosen, which represents Office Professional/Commercial. Because the usage in both the existing condition and the proposed condition are similar, a similar coefficient was used for both conditions. Data was entered into an Excel Spreadsheet which calculates the runoff based on the County of San Diego methodology electronically (County of San Diego Figure 3-1), therefore reducing errors.

For the both the existing and proposed condition the intensity was calculated using the 6 hour and 24 hour 100 year rainfall events for the site area.

The following software packages were used in the analysis of the project:

- Microsoft Excel (Rational Method Hydrology)
- AES Software

Proposed improvements will increase the total peak flow runoff (as compared to existing conditions) in the unmitigated condition. However, through the use of a treatment storage tank and treatment system the project will reduce the peak flow from the site in the mitigated condition.

### **3.2. 100-Year Flow Control**

Hydrographs of the 100-year storm were generated using the RatHydro program. The RatHydro program uses the method outlined in the County of San Diego Hydrology Manual to generate hydrographs consistent with the County of San Diego. These hydrographs were then entered into the Hydraflow Hydrographs as well as the data for the storage tank and outlet. The simulation showed that the 100-year flows were mitigated to below pre-project levels. A copy of the calculations has been included in the appendix of the report.

## Section 4 Results

### 4.1. Hydrologic Results

The following tables summarize the hydrologic analysis of the project. A hydraulic summary of pipe sizing will be completed in conjunction with design of the pump system.

- **Table 1** - summarizes the existing hydrologic properties of the project site.
- **Table 2** - summarizes the proposed condition hydrology of the site in the unmitigated condition.
- **Table 3** - summarizes the proposed condition hydrology of the site in the mitigated condition.
- **Table 4** - compares the existing and proposed mitigated conditions

**Table 1–Existing Condition**

Sub Basin No.	Runoff Coefficient	Basin Intensity (in/hr)	Basin Area (acres)	Runoff (cfs)
Basin A	0.82	5.27	0.47	1.98
Basin B	0.82	5.27	0.53	2.23
<b>TOTALS</b>			<b>1.00</b>	<b>4.21</b>

**Table 2–Proposed Condition (Unmitigated)**

Sub Basin No.	Runoff Coefficient	Basin Intensity (in/hr)	Basin Area (acres)	Runoff (cfs)
Basin A	0.82	5.27	1.00	4.22
<b>TOTALS</b>			<b>1.00</b>	<b>4.22</b>

**Table 3–Proposed Condition (Mitigated)**

Sub Basin No.	Runoff Coefficient	Basin Intensity (in/hr)	Basin Area (acres)	Runoff (cfs)
Basin A	0.82	5.27	1.00	0.22
<b>TOTALS</b>			<b>1.00</b>	<b>0.22</b>

Table 4–Comparison of Flows (Mitigated)

<b>Sub Basin No.</b>	<b>Existing Condition (cfs)</b>	<b>Proposed Condition (cfs)</b>	<b>Difference</b>
Basin A	4.21	0.22	-3.99
<b>TOTALS</b>	<b>4.21</b>	<b>0.22</b>	<b>-3.99</b>

## Section 5 Conclusions

As indicated in Table of Hydrologic Results, the proposed improvements will not increase the total 100-year, 6-hour peak flow rate. In the mitigated condition the flow rate will be 0.223 cfs, a rate less than in the existing condition.

There is not a significant concern for erosion as the site is previously developed. Potential for erosion for the proposed condition shall be minimized by following items listed in the Erosion Control Plan (part of the Rough Grading Plans). Runoff shall flow over relatively flat areas where scour is not a concern. Runoff is not proposed over any sloped areas.

## **Section 6    References**

### **Imperial Beach Municipal Code**

**County of San Diego, 2003.** Hydrology Manual (2003),

**County of San Diego, 2014** Hydraulic Design Manual (2014).

**FEMA, 1997.** FEMA. (June 17, 1997). Flood Insurance Study, San Diego County.

# Appendix A

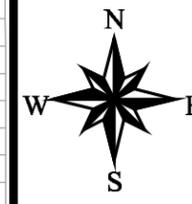
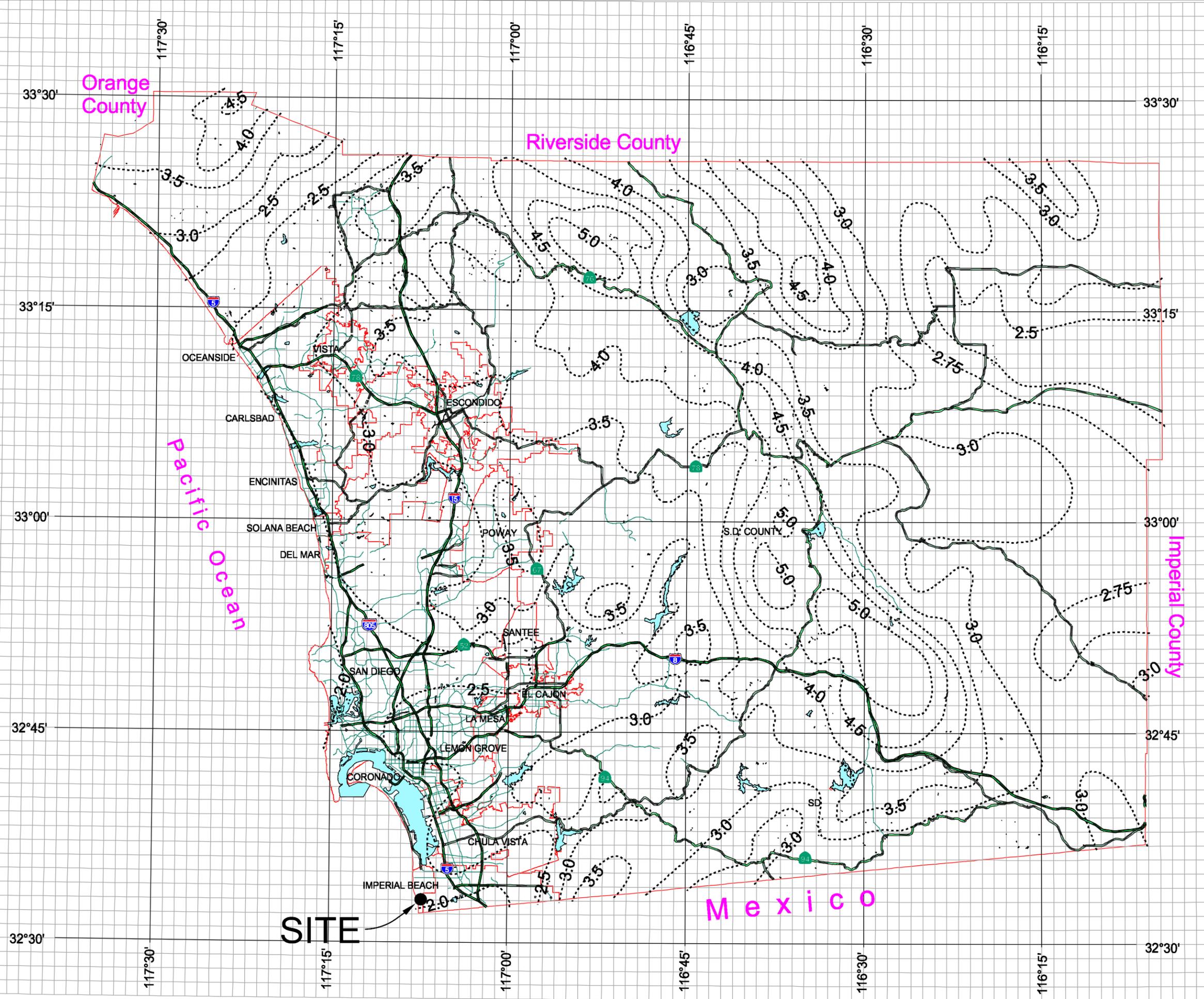
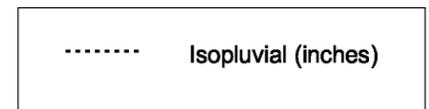
## Rainfall Isopluvials

# County of San Diego Hydrology Manual



## Rainfall Isophvials

### 100 Year Rainfall Event - 6 Hours



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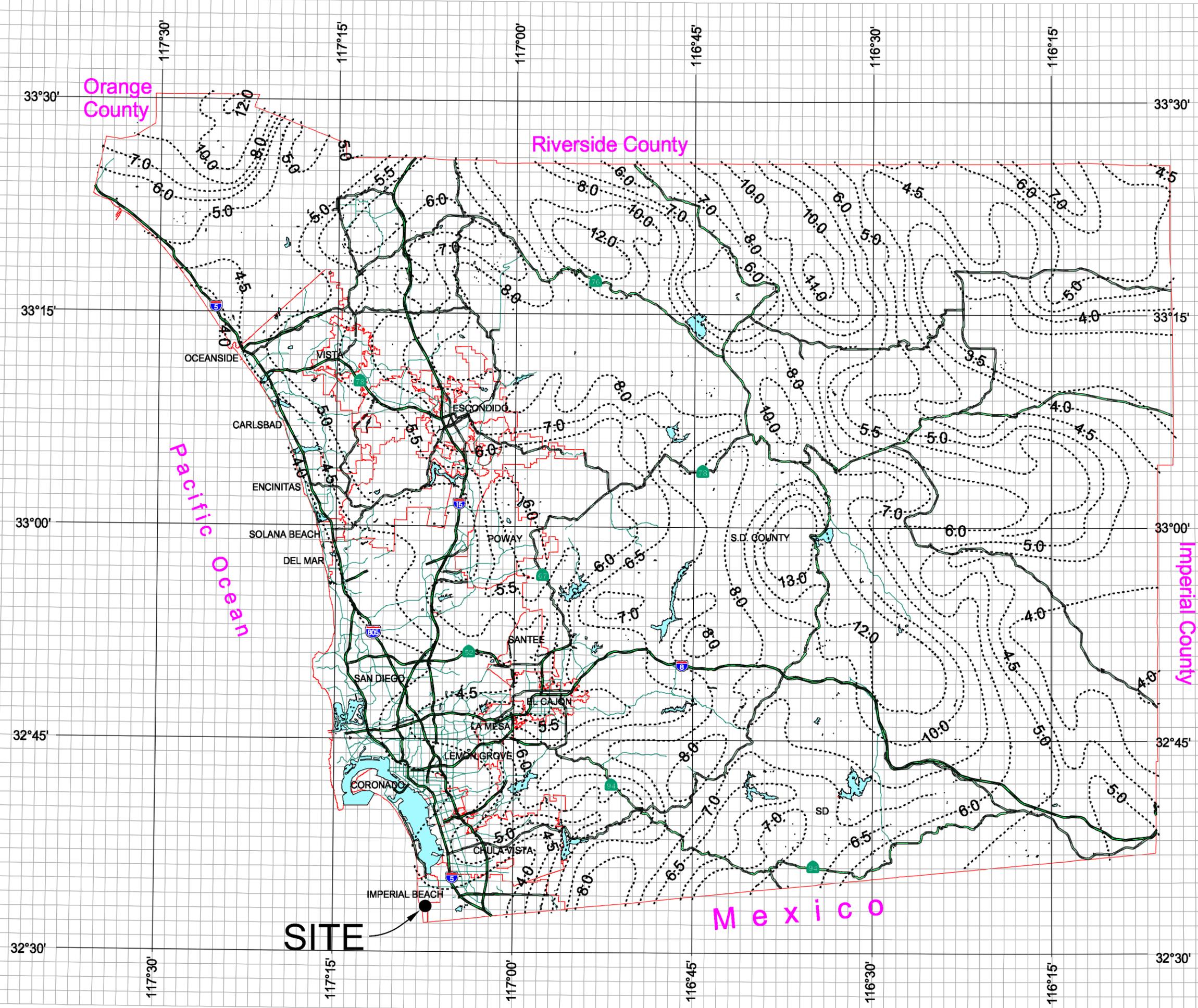
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# County of San Diego Hydrology Manual



## Rainfall Isopluvials

### 100 Year Rainfall Event - 24 Hours



Department of Public Works  
Geographic Information Services

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## Appendix B FEMA Flood Plain Maps



MAP SCALE 1" = 500'

0 250 500 750 1,000 FEET

NFIP

PANEL 2134G

**FIRM**

FLOOD INSURANCE RATE MAP  
SAN DIEGO COUNTY,  
CALIFORNIA  
AND INCORPORATED AREAS

PANEL 2134 OF 2375

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

COMMUNITY	NUMBER	PANEL	SUFFIX
IMPERIAL BEACH, CITY OF	060291	2134	G

Notice to User: The Map Number shown below should be used when placing map orders; the Community Number shown above should be used on insurance applications for the subject community.

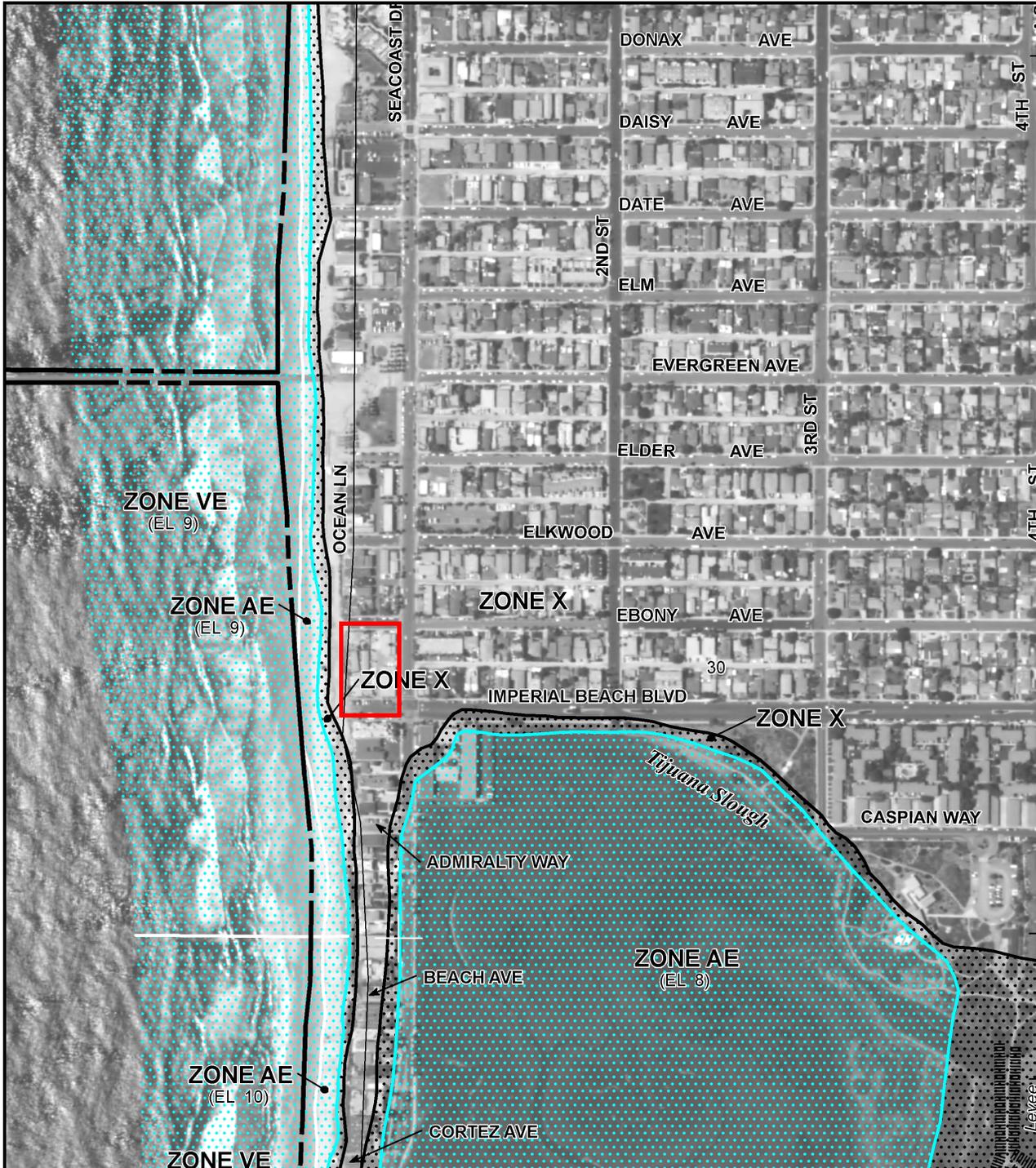
MAP NUMBER  
06073C2134G

MAP REVISED  
MAY 16, 2012



Federal Emergency Management Agency

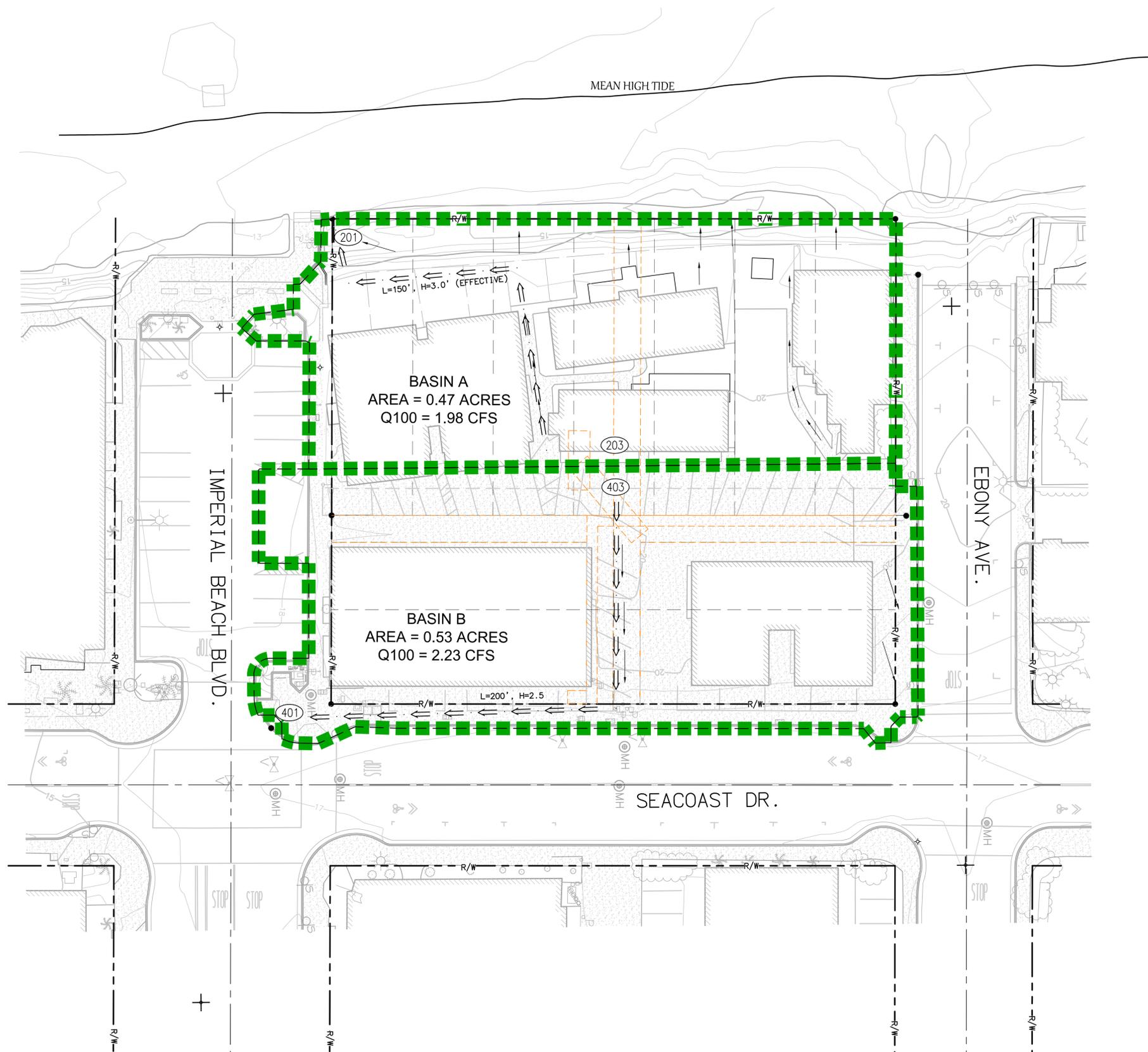
NATIONAL FLOOD INSURANCE PROGRAM



This is an official copy of a portion of the above referenced flood map. It was extracted using F-MIT On-Line. This map does not reflect changes or amendments which may have been made subsequent to the date on the title block. For the latest product information about National Flood Insurance Program flood maps check the FEMA Flood Map Store at [www.msc.fema.gov](http://www.msc.fema.gov)

# Appendix C

## Existing Condition Hydrologic Work Map & Calculations

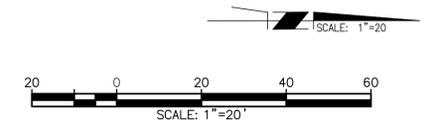


# LEGEND

- LIMITS OF OVERALL NODE [Green dashed line]
- DRAINAGE BASIN FLOW DIRECTION [Arrow]
- EXISTING CONTOUR [Line with 400]
- EXISTING FIRE HYDRANT [Symbol]
- EXISTING STREET LIGHT [Symbol]
- EXISTING CURB [Line]
- FENCE LINE [Dashed line]
- GATE [Symbol]
- SEWER MANHOLE [Symbol]
- SEWER CLEAN OUT [Symbol]
- STORM DRAIN MANHOLE [Symbol]
- DRAIN INLET/CATCH BASIN [Symbol]
- FIRE HYDRANT [Symbol]
- ELECTRIC METER [Symbol]
- ELECTRIC PULL BOX [Symbol]
- POWER POLE [Symbol]
- AREA LIGHT [Symbol]
- STREET LIGHT [Symbol]
- BACK FLOW PREVENTER [Symbol]
- TELEPHONE VAULT [Symbol]
- ELECTRIC TRANSFORMER [Symbol]
- WATER VAULT [Symbol]

## IMPERIAL BEACH RESORT 1046 SEACOAST DR. IMPERIAL BEACH, CA EXISTING CONDITIONS DRAINAGE AREAS

02 /16/17



**Michael Baker**  
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San Diego, CA 92124  
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\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
2003,1985,1981 HYDROLOGY MANUAL
(c) Copyright 1982-2013 Advanced Engineering Software (aes)
Ver. 20.0 Release Date: 06/01/2013 License ID 1264

Analysis prepared by:

Michael Baker International
9755 Clairemont Mesa Blvd.
San Diego, CA 92124

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*
\* Imperial Beach Resort \*
\* 100-year Flows \*
\* February 16, 2017 \*
\*\*\*\*\*

FILE NAME: C:\IB\EX.DAT
TIME/DATE OF STUDY: 14:40 02/16/2017

-----
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
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2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00
6-HOUR DURATION PRECIPITATION (INCHES) = 2.000
SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

Table with 10 columns: NO., HALF-WIDTH (FT), CROWN TO CROSSFALL (FT), STREET-CROSSFALL: IN-SIDE / OUT-SIDE / PARK-WAY, CURB HEIGHT (FT), GUTTER WIDTH (FT), GUTTER LIP (FT), GUTTER HIKE (FT), GUTTER GEOMETRIES: MANNING FACTOR (n). Row 1: 1, 30.0, 20.0, 0.018/0.018/0.020, 0.67, 2.00, 0.0313, 0.167, 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)
\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*
FLOW PROCESS FROM NODE 203.00 TO NODE 201.00 IS CODE = 21
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

-----
GENERAL COMMERCIAL RUNOFF COEFFICIENT = .8000
SOIL CLASSIFICATION IS "B"
S.C.S. CURVE NUMBER (AMC II) = 92
INITIAL SUBAREA FLOW-LENGTH(FEET) = 150.00
UPSTREAM ELEVATION(FEET) = 21.00
DOWNSTREAM ELEVATION(FEET) = 18.00

ELEVATION DIFFERENCE(FEET) = 3.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.712  
 WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
 THE MAXIMUM OVERLAND FLOW LENGTH = 75.00  
 (Reference: Table 3-1B of Hydrology Manual)  
 THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.269  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 1.98  
 TOTAL AREA(ACRES) = 0.47 TOTAL RUNOFF(CFS) = 1.98

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 403.00 TO NODE 401.00 IS CODE = 21

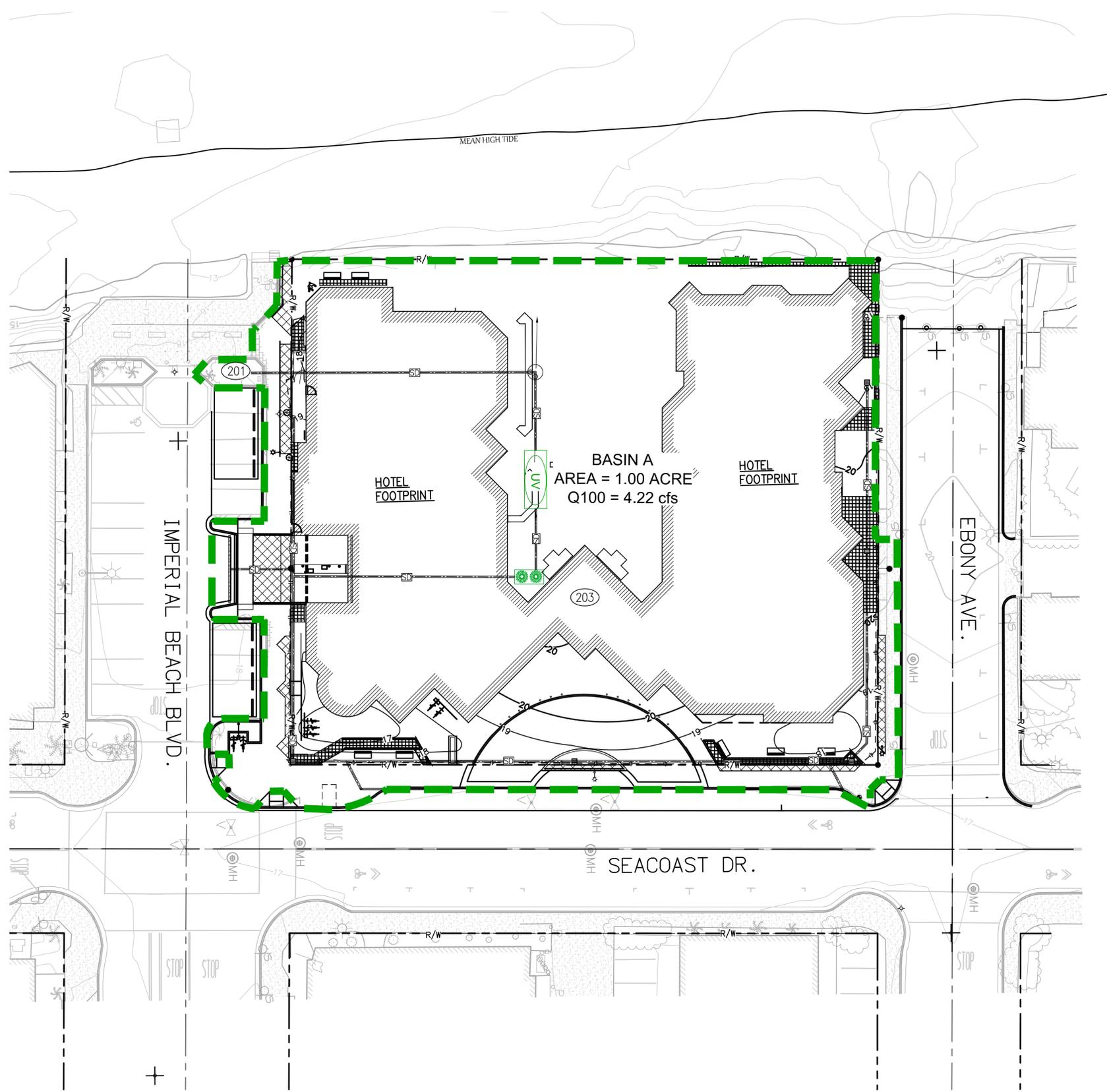
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

GENERAL COMMERCIAL RUNOFF COEFFICIENT = .8000  
 SOIL CLASSIFICATION IS "B"  
 S.C.S. CURVE NUMBER (AMC II) = 92  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 200.00  
 UPSTREAM ELEVATION(FEET) = 20.00  
 DOWNSTREAM ELEVATION(FEET) = 17.50  
 ELEVATION DIFFERENCE(FEET) = 2.50  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.003  
 WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
 THE MAXIMUM OVERLAND FLOW LENGTH = 63.75  
 (Reference: Table 3-1B of Hydrology Manual)  
 THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.269  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 2.23  
 TOTAL AREA(ACRES) = 0.53 TOTAL RUNOFF(CFS) = 2.23

END OF STUDY SUMMARY:  
 TOTAL AREA(ACRES) = 0.5 TC(MIN.) = 4.00  
 PEAK FLOW RATE(CFS) = 2.23

END OF RATIONAL METHOD ANALYSIS

Appendix D  
Proposed Condition Hydrologic  
Work Map & Calculations



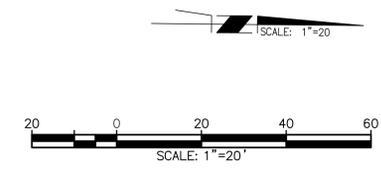
# LEGEND

- LIMITS OF OVERALL NODE [Dashed Green Line]
- DRAINAGE BASIN (XXX)
- FLOW DIRECTION [Arrow]
- EXISTING CONTOUR [Line with 400]
- EXISTING FIRE HYDRANT [Hydrant Symbol]
- EXISTING STREET LIGHT [Street Light Symbol]
- EXISTING CURB [Curb Line]
- FENCE LINE [Dashed Line]
- GATE [Gate Symbol]
- SEWER MANHOLE [Sewer MH Symbol]
- SEWER CLEAN OUT [Sewer CO Symbol]
- STORM DRAIN MANHOLE [Storm Drain MH Symbol]
- DRAIN INLET/CATCH BASIN [Drain Inlet Symbol]
- FIRE HYDRANT [Fire Hydrant Symbol]
- ELECTRIC METER [Electric Meter Symbol]
- ELECTRIC PULL BOX [Electric Pull Box Symbol]
- POWER POLE [Power Pole Symbol]
- AREA LIGHT [Area Light Symbol]
- STREET LIGHT [Street Light Symbol]
- BACK FLOW PREVENTER BFP
- TELEPHONE VAULT TELVLT
- ELECTRIC TRANSFORMER TRANS
- WATER VAULT WVLT

## IMPERIAL BEACH RESORT 1046 SEACOAST DR. IMPERIAL BEACH, CA PROPOSED CONDITIONS DRAINAGE AREAS

02 /16/17

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\*\*\*\*\*

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Ver. 20.0 Release Date: 06/01/2013 License ID 1264

Analysis prepared by:

Michael Baker International
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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* Imperial Beach Resort \*
\* 100-Year Flows \*
\* February 16, 2017 \*
\*\*\*\*\*

FILE NAME: C:\IB\PR.DAT
TIME/DATE OF STUDY: 14:41 02/16/2017

-----
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00
6-HOUR DURATION PRECIPITATION (INCHES) = 2.000
SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

Table with 10 columns: NO., HALF-WIDTH (FT), CROWN TO CROSSFALL (FT), STREET-CROSSFALL: IN-SIDE / OUT-SIDE / PARK-WAY, CURB HEIGHT (FT), GUTTER WIDTH (FT), GUTTER LIP (FT), GUTTER HIKE (FT), GUTTER GEOMETRIES: MANNING FACTOR (n). Row 1: 1, 30.0, 20.0, 0.018/0.018/0.020, 0.67, 2.00, 0.0312, 0.167, 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

- 1. Relative Flow-Depth = 0.00 FEET as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 203.00 TO NODE 201.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

GENERAL COMMERCIAL RUNOFF COEFFICIENT = .8000
SOIL CLASSIFICATION IS "B"
S.C.S. CURVE NUMBER (AMC II) = 92
INITIAL SUBAREA FLOW-LENGTH(FEET) = 200.00
UPSTREAM ELEVATION(FEET) = 21.00
DOWNSTREAM ELEVATION(FEET) = 19.00

ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.183  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 60.00  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.269  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 4.22  
TOTAL AREA(ACRES) = 1.00 TOTAL RUNOFF(CFS) = 4.22

=====  
END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 1.0 TC(MIN.) = 4.18  
PEAK FLOW RATE(CFS) = 4.22

=====  
END OF RATIONAL METHOD ANALYSIS

RUN DATE 2/16/2017  
HYDROGRAPH FILE NAME Text1  
TIME OF CONCENTRATION 5 MIN.  
6 HOUR RAINFALL 2 INCHES  
BASIN AREA 1 ACRES  
RUNOFF COEFFICIENT 0.82  
PEAK DISCHARGE 4.22 CFS

TIME (MIN) = 0	DISCHARGE (CFS) = 0
TIME (MIN) = 5	DISCHARGE (CFS) = 0.1
TIME (MIN) = 10	DISCHARGE (CFS) = 0.1
TIME (MIN) = 15	DISCHARGE (CFS) = 0.1
TIME (MIN) = 20	DISCHARGE (CFS) = 0.1
TIME (MIN) = 25	DISCHARGE (CFS) = 0.1
TIME (MIN) = 30	DISCHARGE (CFS) = 0.1
TIME (MIN) = 35	DISCHARGE (CFS) = 0.1
TIME (MIN) = 40	DISCHARGE (CFS) = 0.1
TIME (MIN) = 45	DISCHARGE (CFS) = 0.1
TIME (MIN) = 50	DISCHARGE (CFS) = 0.1
TIME (MIN) = 55	DISCHARGE (CFS) = 0.1
TIME (MIN) = 60	DISCHARGE (CFS) = 0.1
TIME (MIN) = 65	DISCHARGE (CFS) = 0.1
TIME (MIN) = 70	DISCHARGE (CFS) = 0.1
TIME (MIN) = 75	DISCHARGE (CFS) = 0.1
TIME (MIN) = 80	DISCHARGE (CFS) = 0.1
TIME (MIN) = 85	DISCHARGE (CFS) = 0.1
TIME (MIN) = 90	DISCHARGE (CFS) = 0.1
TIME (MIN) = 95	DISCHARGE (CFS) = 0.1
TIME (MIN) = 100	DISCHARGE (CFS) = 0.1
TIME (MIN) = 105	DISCHARGE (CFS) = 0.1
TIME (MIN) = 110	DISCHARGE (CFS) = 0.1
TIME (MIN) = 115	DISCHARGE (CFS) = 0.1
TIME (MIN) = 120	DISCHARGE (CFS) = 0.1
TIME (MIN) = 125	DISCHARGE (CFS) = 0.2
TIME (MIN) = 130	DISCHARGE (CFS) = 0.2
TIME (MIN) = 135	DISCHARGE (CFS) = 0.2
TIME (MIN) = 140	DISCHARGE (CFS) = 0.2
TIME (MIN) = 145	DISCHARGE (CFS) = 0.2
TIME (MIN) = 150	DISCHARGE (CFS) = 0.2
TIME (MIN) = 155	DISCHARGE (CFS) = 0.2
TIME (MIN) = 160	DISCHARGE (CFS) = 0.2
TIME (MIN) = 165	DISCHARGE (CFS) = 0.2
TIME (MIN) = 170	DISCHARGE (CFS) = 0.2
TIME (MIN) = 175	DISCHARGE (CFS) = 0.2
TIME (MIN) = 180	DISCHARGE (CFS) = 0.2
TIME (MIN) = 185	DISCHARGE (CFS) = 0.2
TIME (MIN) = 190	DISCHARGE (CFS) = 0.3
TIME (MIN) = 195	DISCHARGE (CFS) = 0.3
TIME (MIN) = 200	DISCHARGE (CFS) = 0.3
TIME (MIN) = 205	DISCHARGE (CFS) = 0.3
TIME (MIN) = 210	DISCHARGE (CFS) = 0.3
TIME (MIN) = 215	DISCHARGE (CFS) = 0.4
TIME (MIN) = 220	DISCHARGE (CFS) = 0.4
TIME (MIN) = 225	DISCHARGE (CFS) = 0.5
TIME (MIN) = 230	DISCHARGE (CFS) = 0.6
TIME (MIN) = 235	DISCHARGE (CFS) = 0.9
TIME (MIN) = 240	DISCHARGE (CFS) = 1.3
TIME (MIN) = 245	DISCHARGE (CFS) = 4.22
TIME (MIN) = 250	DISCHARGE (CFS) = 0.7
TIME (MIN) = 255	DISCHARGE (CFS) = 0.5
TIME (MIN) = 260	DISCHARGE (CFS) = 0.4
TIME (MIN) = 265	DISCHARGE (CFS) = 0.3
TIME (MIN) = 270	DISCHARGE (CFS) = 0.3
TIME (MIN) = 275	DISCHARGE (CFS) = 0.2
TIME (MIN) = 280	DISCHARGE (CFS) = 0.2
TIME (MIN) = 285	DISCHARGE (CFS) = 0.2
TIME (MIN) = 290	DISCHARGE (CFS) = 0.2
TIME (MIN) = 295	DISCHARGE (CFS) = 0.2
TIME (MIN) = 300	DISCHARGE (CFS) = 0.2
TIME (MIN) = 305	DISCHARGE (CFS) = 0.2
TIME (MIN) = 310	DISCHARGE (CFS) = 0.1
TIME (MIN) = 315	DISCHARGE (CFS) = 0.1
TIME (MIN) = 320	DISCHARGE (CFS) = 0.1
TIME (MIN) = 325	DISCHARGE (CFS) = 0.1
TIME (MIN) = 330	DISCHARGE (CFS) = 0.1
TIME (MIN) = 335	DISCHARGE (CFS) = 0.1
TIME (MIN) = 340	DISCHARGE (CFS) = 0.1
TIME (MIN) = 345	DISCHARGE (CFS) = 0.1
TIME (MIN) = 350	DISCHARGE (CFS) = 0.1
TIME (MIN) = 355	DISCHARGE (CFS) = 0.1
TIME (MIN) = 360	DISCHARGE (CFS) = 0.1
TIME (MIN) = 365	DISCHARGE (CFS) = 0

# Watershed Model Schematic

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5



## Legend

<u>Hyd.</u>	<u>Origin</u>	<u>Description</u>
1	Manual	Input Hydrograph
2	Reservoir	Outflow Hydrograph

# Hydrograph Return Period Recap

Hydroflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Hyd. No.	Hydrograph type (origin)	Inflow hyd(s)	Peak Outflow (cfs)								Hydrograph Description
			1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	
1	Manual	-----	-----	-----	-----	-----	-----	-----	-----	4.220	Input Hydrograph
2	Reservoir	1	-----	-----	-----	-----	-----	-----	-----	0.223	Outflow Hydrograph
Proj. file: Hydrology.gpw										Thursday, 02 / 16 / 2017	

# Hydrograph Summary Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	Manual	4.220	5	245	5,826	-----	-----	-----	Input Hydrograph
2	Reservoir	0.223	5	195	5,825	1	103.89	2,614	Outflow Hydrograph
Hydrology.gpw					Return Period: 100 Year			Thursday, 02 / 16 / 2017	

# Hydrograph Report

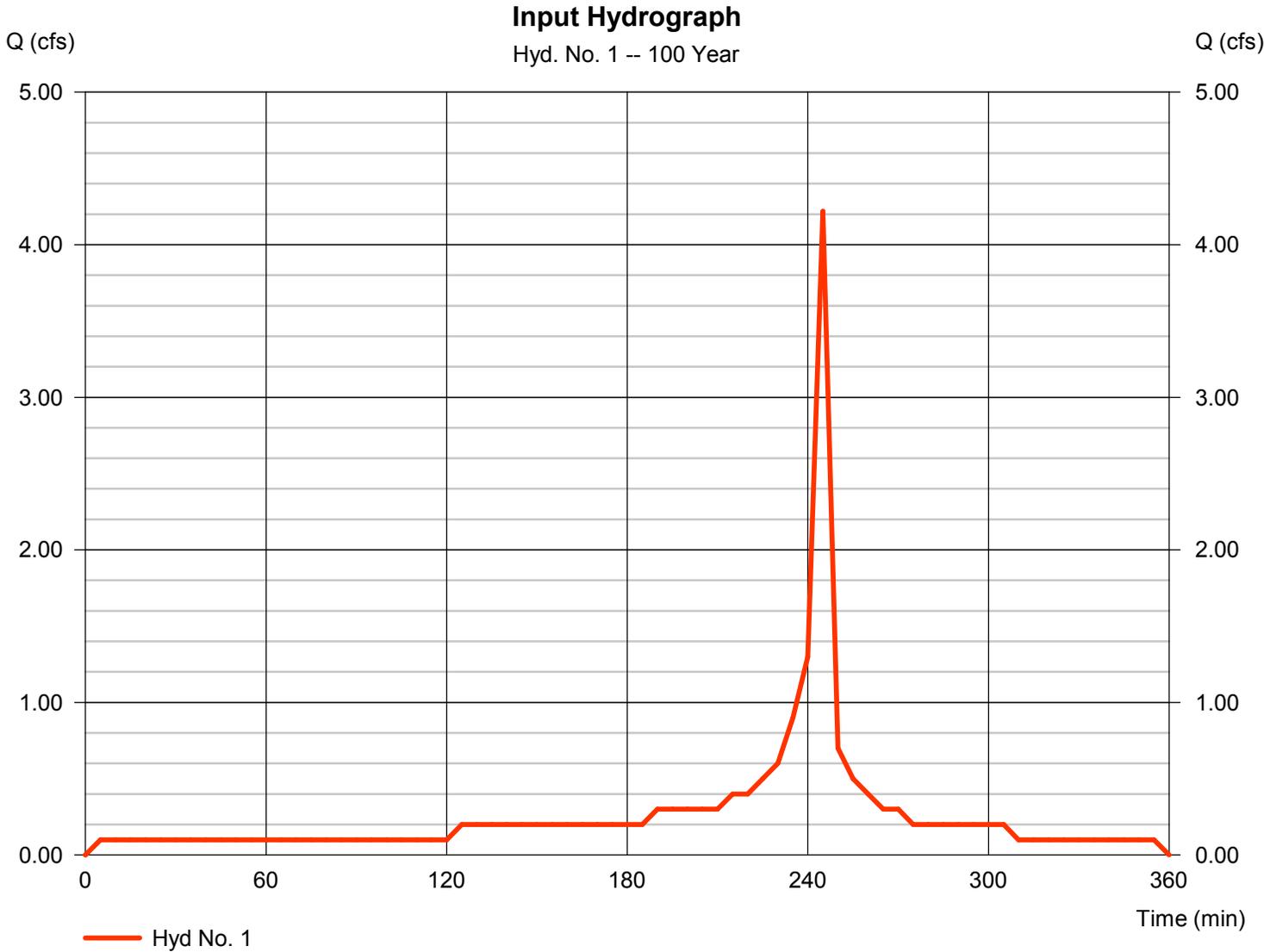
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 02 / 16 / 2017

## Hyd. No. 1

### Input Hydrograph

Hydrograph type	= Manual	Peak discharge	= 4.220 cfs
Storm frequency	= 100 yrs	Time to peak	= 245 min
Time interval	= 5 min	Hyd. volume	= 5,826 cuft



# Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

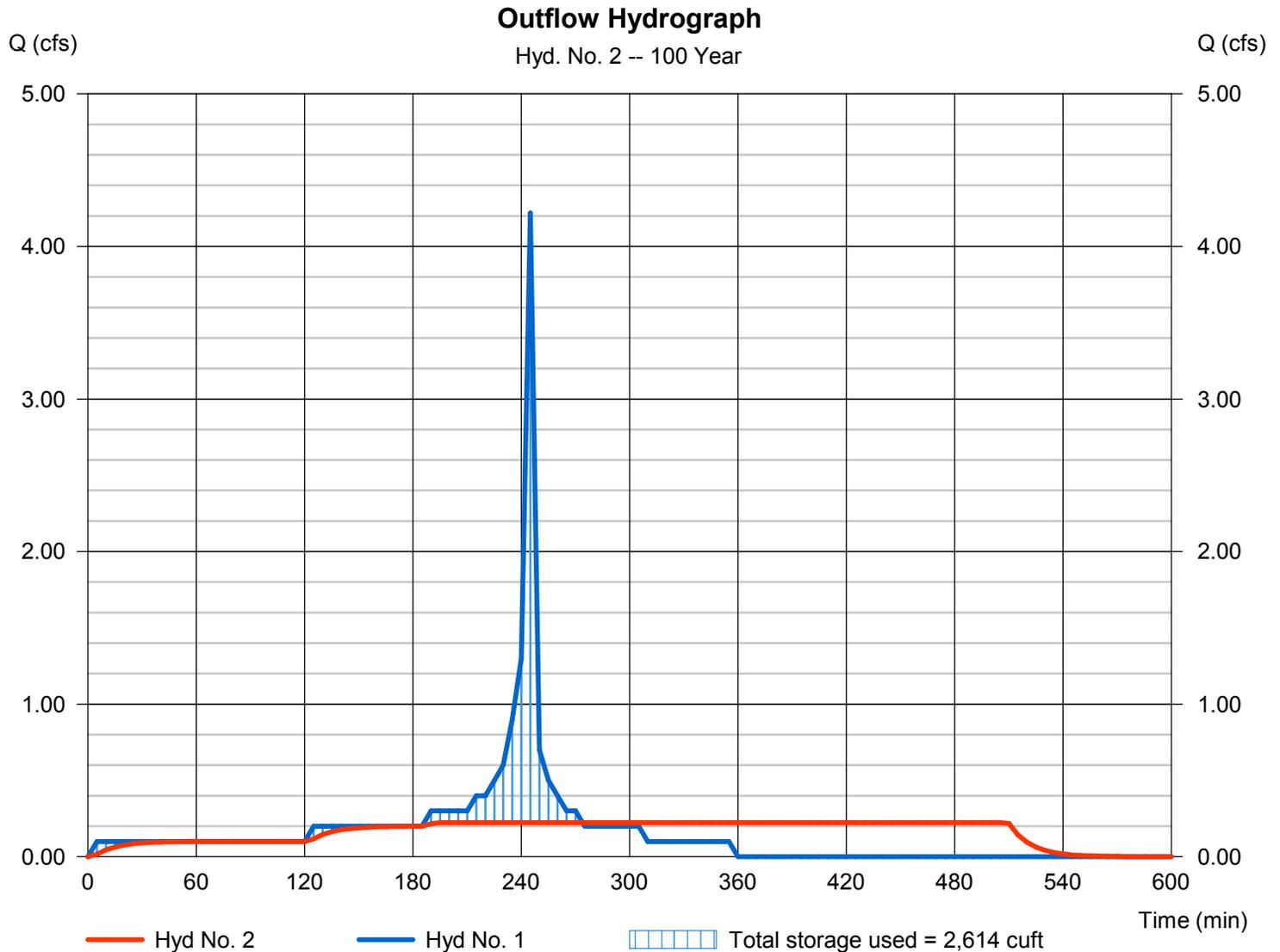
Thursday, 02 / 16 / 2017

## Hyd. No. 2

### Outflow Hydrograph

Hydrograph type	= Reservoir	Peak discharge	= 0.223 cfs
Storm frequency	= 100 yrs	Time to peak	= 195 min
Time interval	= 5 min	Hyd. volume	= 5,825 cuft
Inflow hyd. No.	= 1 - Input Hydrograph	Max. Elevation	= 103.89 ft
Reservoir name	= Storage Tank	Max. Storage	= 2,614 cuft

Storage Indication method used.



# Hydrograph Report

## Hyd. No. 1

### Input Hydrograph

Hydrograph type	= Manual	Peak discharge	= 4.220 cfs
Storm frequency	= 100 yrs	Time to peak	= 4.08 hrs
Time interval	= 5 min	Hyd. volume	= 5,826 cuft

### Hydrograph Discharge Table

(Printed values >= 1.00% of Qp.)

Time -- Outflow	Time -- Outflow	Time -- Outflow	Time -- Outflow
(hrs cfs)	(hrs cfs)	(hrs cfs)	(hrs cfs)
0.08 0.100	1.83 0.100	3.58 0.400	5.33 0.100
0.17 0.100	1.92 0.100	3.67 0.400	5.42 0.100
0.25 0.100	2.00 0.100	3.75 0.500	5.50 0.100
0.33 0.100	2.08 0.200	3.83 0.600	5.58 0.100
0.42 0.100	2.17 0.200	3.92 0.900	5.67 0.100
0.50 0.100	2.25 0.200	4.00 1.300	5.75 0.100
0.58 0.100	2.33 0.200	4.08 4.220	5.83 0.100
0.67 0.100	2.42 0.200	4.17 0.700	5.92 0.100
0.75 0.100	2.50 0.200	4.25 0.500	...End
0.83 0.100	2.58 0.200	4.33 0.400	
0.92 0.100	2.67 0.200	4.42 0.300	
1.00 0.100	2.75 0.200	4.50 0.300	
1.08 0.100	2.83 0.200	4.58 0.200	
1.17 0.100	2.92 0.200	4.67 0.200	
1.25 0.100	3.00 0.200	4.75 0.200	
1.33 0.100	3.08 0.200	4.83 0.200	
1.42 0.100	3.17 0.300	4.92 0.200	
1.50 0.100	3.25 0.300	5.00 0.200	
1.58 0.100	3.33 0.300	5.08 0.200	
1.67 0.100	3.42 0.300	5.17 0.100	
1.75 0.100	3.50 0.300	5.25 0.100	

<<

# Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 02 / 16 / 2017

## Hyd. No. 2

### Outflow Hydrograph

Hydrograph type	= Reservoir	Peak discharge	= 0.223 cfs
Storm frequency	= 100 yrs	Time to peak	= 3.25 hrs
Time interval	= 5 min	Hyd. volume	= 5,825 cuft
Inflow hyd. No.	= 1 - Input Hydrograph	Reservoir name	= Storage Tank
Max. Elevation	= 103.89 ft	Max. Storage	= 2,614 cuft

Storage Indication method used.

### Hydrograph Discharge Table

(Printed values &gt;= 1.00% of Qp.)

Time (hrs)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
0.08	0.100	100.04	----	----	----	----	----	----	----	----	----	0.017
0.17	0.100	100.10	----	----	----	----	----	----	----	----	----	0.045
0.25	0.100	100.14	----	----	----	----	----	----	----	----	----	0.064
0.33	0.100	100.17	----	----	----	----	----	----	----	----	----	0.076
0.42	0.100	100.19	----	----	----	----	----	----	----	----	----	0.084
0.50	0.100	100.20	----	----	----	----	----	----	----	----	----	0.090
0.58	0.100	100.21	----	----	----	----	----	----	----	----	----	0.093
0.67	0.100	100.21	----	----	----	----	----	----	----	----	----	0.095
0.75	0.100	100.22	----	----	----	----	----	----	----	----	----	0.097
0.83	0.100	100.22	----	----	----	----	----	----	----	----	----	0.098
0.92	0.100	100.22	----	----	----	----	----	----	----	----	----	0.099
1.00	0.100	100.22	----	----	----	----	----	----	----	----	----	0.099
1.08	0.100	100.22	----	----	----	----	----	----	----	----	----	0.099
1.17	0.100	100.22	----	----	----	----	----	----	----	----	----	0.100
1.25	0.100	100.22	----	----	----	----	----	----	----	----	----	0.100
1.33	0.100	100.22	----	----	----	----	----	----	----	----	----	0.100
1.42	0.100	100.22	----	----	----	----	----	----	----	----	----	0.100
1.50	0.100	100.22	----	----	----	----	----	----	----	----	----	0.100
1.58	0.100	100.22	----	----	----	----	----	----	----	----	----	0.100
1.67	0.100	100.22	----	----	----	----	----	----	----	----	----	0.100

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Outflow Hydrograph

Hydrograph Discharge Table

Time (hrs)	Inflow cfs	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Outflow cfs
<< 7.00	0.000	100.50 <<	----	----	----	----	----	----	----	----	----	0.223
<< 7.08	0.000	100.50 <<	----	----	----	----	----	----	----	----	----	0.223
<< 7.17	0.000	100.50 <<	----	----	----	----	----	----	----	----	----	0.223
<< 7.25	0.000	100.50 <<	----	----	----	----	----	----	----	----	----	0.223
<< 7.33	0.000	100.50 <<	----	----	----	----	----	----	----	----	----	0.223
<< 7.42	0.000	100.50 <<	----	----	----	----	----	----	----	----	----	0.223
<< 7.50	0.000	100.50 <<	----	----	----	----	----	----	----	----	----	0.223
<< 7.58	0.000	100.50 <<	----	----	----	----	----	----	----	----	----	0.223
<< 7.67	0.000	100.50 <<	----	----	----	----	----	----	----	----	----	0.223
<< 7.75	0.000	100.50 <<	----	----	----	----	----	----	----	----	----	0.223
<< 7.83	0.000	100.50 <<	----	----	----	----	----	----	----	----	----	0.223
<< 7.92	0.000	100.50 <<	----	----	----	----	----	----	----	----	----	0.223
<< 8.00	0.000	100.50 <<	----	----	----	----	----	----	----	----	----	0.223
<< 8.08	0.000	100.50 <<	----	----	----	----	----	----	----	----	----	0.223
<< 8.17	0.000	100.50 <<	----	----	----	----	----	----	----	----	----	0.223
<< 8.25	0.000	100.50 <<	----	----	----	----	----	----	----	----	----	0.223
<< 8.33	0.000	100.50 <<	----	----	----	----	----	----	----	----	----	0.223
<< 8.42	0.000	100.50 <<	----	----	----	----	----	----	----	----	----	0.223
8.50	0.000	100.49	----	----	----	----	----	----	----	----	----	0.218

Continues on next page...

Outflow Hydrograph

**Hydrograph Discharge Table**

<b>Time (hrs)</b>	<b>Inflow cfs</b>	<b>Elevation ft</b>	<b>Clv A cfs</b>	<b>Clv B cfs</b>	<b>Clv C cfs</b>	<b>PfRsr cfs</b>	<b>Wr A cfs</b>	<b>Wr B cfs</b>	<b>Wr C cfs</b>	<b>Wr D cfs</b>	<b>Exfil cfs</b>	<b>Outflow cfs</b>
8.58	0.000	100.32	----	----	----	----	----	----	----	----	----	0.144
8.67	0.000	100.21	----	----	----	----	----	----	----	----	----	0.095
8.75	0.000	100.14	----	----	----	----	----	----	----	----	----	0.063
8.83	0.000	100.09	----	----	----	----	----	----	----	----	----	0.041
8.92	0.000	100.06	----	----	----	----	----	----	----	----	----	0.027
9.00	0.000	100.04	----	----	----	----	----	----	----	----	----	0.018
9.08	0.000	100.03	----	----	----	----	----	----	----	----	----	0.012
9.17	0.000	100.02	----	----	----	----	----	----	----	----	----	0.008
9.25	0.000	100.01	----	----	----	----	----	----	----	----	----	0.005
9.33	0.000	100.01	----	----	----	----	----	----	----	----	----	0.003
9.42	0.000	100.01	----	----	----	----	----	----	----	----	----	0.002

...End

# Pond Report

## Pond No. 1 - Storage Tank

### Pond Data

UG Chambers -Invert elev. = 100.00 ft, Rise x Span = 5.00 x 5.00 ft, Barrel Len = 160.00 ft, No. Barrels = 1, Slope = 0.00%, Headers = No

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	100.00	n/a	0	0
0.50	100.50	n/a	164	164
1.00	101.00	n/a	284	448
1.50	101.50	n/a	346	793
2.00	102.00	n/a	381	1,174
2.50	102.50	n/a	398	1,571
3.00	103.00	n/a	398	1,969
3.50	103.50	n/a	381	2,350
4.00	104.00	n/a	345	2,695
4.50	104.50	n/a	284	2,979
5.00	105.00	n/a	163	3,142

### Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 0.00	0.00	0.00	0.00
Span (in)	= 0.00	0.00	0.00	0.00
No. Barrels	= 0	0	0	0
Invert El. (ft)	= 0.00	0.00	0.00	0.00
Length (ft)	= 0.00	0.00	0.00	0.00
Slope (%)	= 0.00	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

### Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 0.00	0.00	0.00	0.00
Crest El. (ft)	= 0.00	0.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	3.33	3.33
Weir Type	= ---	---	---	---
Multi-Stage	= No	No	No	No
Exfil.(in/hr)	= 0.000 (by Contour)			
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

### Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	100.00	---	---	---	---	---	---	---	---	---	---	0.000
0.05	16	100.05	---	---	---	---	---	---	---	---	---	0.022	0.022
0.10	33	100.10	---	---	---	---	---	---	---	---	---	0.045	0.045
0.15	49	100.15	---	---	---	---	---	---	---	---	---	0.067	0.067
0.20	65	100.20	---	---	---	---	---	---	---	---	---	0.089	0.089
0.25	82	100.25	---	---	---	---	---	---	---	---	---	0.112	0.112
0.30	98	100.30	---	---	---	---	---	---	---	---	---	0.134	0.134
0.35	114	100.35	---	---	---	---	---	---	---	---	---	0.156	0.156
0.40	131	100.40	---	---	---	---	---	---	---	---	---	0.178	0.178
0.45	147	100.45	---	---	---	---	---	---	---	---	---	0.201	0.201
0.50	164	100.50	---	---	---	---	---	---	---	---	---	0.223	0.223
0.55	192	100.55	---	---	---	---	---	---	---	---	---	0.223	0.223
0.60	220	100.60	---	---	---	---	---	---	---	---	---	0.223	0.223
0.65	249	100.65	---	---	---	---	---	---	---	---	---	0.223	0.223
0.70	277	100.70	---	---	---	---	---	---	---	---	---	0.223	0.223
0.75	306	100.75	---	---	---	---	---	---	---	---	---	0.223	0.223
0.80	334	100.80	---	---	---	---	---	---	---	---	---	0.223	0.223
0.85	362	100.85	---	---	---	---	---	---	---	---	---	0.223	0.223
0.90	391	100.90	---	---	---	---	---	---	---	---	---	0.223	0.223
0.95	419	100.95	---	---	---	---	---	---	---	---	---	0.223	0.223
1.00	448	101.00	---	---	---	---	---	---	---	---	---	0.223	0.223
1.05	482	101.05	---	---	---	---	---	---	---	---	---	0.223	0.223
1.10	517	101.10	---	---	---	---	---	---	---	---	---	0.223	0.223
1.15	551	101.15	---	---	---	---	---	---	---	---	---	0.223	0.223
1.20	586	101.20	---	---	---	---	---	---	---	---	---	0.223	0.223
1.25	620	101.25	---	---	---	---	---	---	---	---	---	0.223	0.223
1.30	655	101.30	---	---	---	---	---	---	---	---	---	0.223	0.223
1.35	690	101.35	---	---	---	---	---	---	---	---	---	0.223	0.223
1.40	724	101.40	---	---	---	---	---	---	---	---	---	0.223	0.223
1.45	759	101.45	---	---	---	---	---	---	---	---	---	0.223	0.223
1.50	793	101.50	---	---	---	---	---	---	---	---	---	0.223	0.223
1.55	831	101.55	---	---	---	---	---	---	---	---	---	0.223	0.223

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Storage Tank

**Stage / Storage / Discharge Table**

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
1.60	869	101.60	---	---	---	---	---	---	---	---	---	0.223	0.223
1.65	907	101.65	---	---	---	---	---	---	---	---	---	0.223	0.223
1.70	945	101.70	---	---	---	---	---	---	---	---	---	0.223	0.223
1.75	984	101.75	---	---	---	---	---	---	---	---	---	0.223	0.223
1.80	1,022	101.80	---	---	---	---	---	---	---	---	---	0.223	0.223
1.85	1,060	101.85	---	---	---	---	---	---	---	---	---	0.223	0.223
1.90	1,098	101.90	---	---	---	---	---	---	---	---	---	0.223	0.223
1.95	1,136	101.95	---	---	---	---	---	---	---	---	---	0.223	0.223
2.00	1,174	102.00	---	---	---	---	---	---	---	---	---	0.223	0.223
2.05	1,214	102.05	---	---	---	---	---	---	---	---	---	0.223	0.223
2.10	1,253	102.10	---	---	---	---	---	---	---	---	---	0.223	0.223
2.15	1,293	102.15	---	---	---	---	---	---	---	---	---	0.223	0.223
2.20	1,333	102.20	---	---	---	---	---	---	---	---	---	0.223	0.223
2.25	1,373	102.25	---	---	---	---	---	---	---	---	---	0.223	0.223
2.30	1,412	102.30	---	---	---	---	---	---	---	---	---	0.223	0.223
2.35	1,452	102.35	---	---	---	---	---	---	---	---	---	0.223	0.223
2.40	1,492	102.40	---	---	---	---	---	---	---	---	---	0.223	0.223
2.45	1,532	102.45	---	---	---	---	---	---	---	---	---	0.223	0.223
2.50	1,571	102.50	---	---	---	---	---	---	---	---	---	0.223	0.223
2.55	1,611	102.55	---	---	---	---	---	---	---	---	---	0.223	0.223
2.60	1,651	102.60	---	---	---	---	---	---	---	---	---	0.223	0.223
2.65	1,691	102.65	---	---	---	---	---	---	---	---	---	0.223	0.223
2.70	1,731	102.70	---	---	---	---	---	---	---	---	---	0.223	0.223
2.75	1,770	102.75	---	---	---	---	---	---	---	---	---	0.223	0.223
2.80	1,810	102.80	---	---	---	---	---	---	---	---	---	0.223	0.223
2.85	1,850	102.85	---	---	---	---	---	---	---	---	---	0.223	0.223
2.90	1,890	102.90	---	---	---	---	---	---	---	---	---	0.223	0.223
2.95	1,929	102.95	---	---	---	---	---	---	---	---	---	0.223	0.223
3.00	1,969	103.00	---	---	---	---	---	---	---	---	---	0.223	0.223
3.05	2,007	103.05	---	---	---	---	---	---	---	---	---	0.223	0.223
3.10	2,045	103.10	---	---	---	---	---	---	---	---	---	0.223	0.223
3.15	2,083	103.15	---	---	---	---	---	---	---	---	---	0.223	0.223
3.20	2,121	103.20	---	---	---	---	---	---	---	---	---	0.223	0.223
3.25	2,159	103.25	---	---	---	---	---	---	---	---	---	0.223	0.223
3.30	2,197	103.30	---	---	---	---	---	---	---	---	---	0.223	0.223
3.35	2,235	103.35	---	---	---	---	---	---	---	---	---	0.223	0.223
3.40	2,274	103.40	---	---	---	---	---	---	---	---	---	0.223	0.223
3.45	2,312	103.45	---	---	---	---	---	---	---	---	---	0.223	0.223
3.50	2,350	103.50	---	---	---	---	---	---	---	---	---	0.223	0.223
3.55	2,384	103.55	---	---	---	---	---	---	---	---	---	0.223	0.223
3.60	2,419	103.60	---	---	---	---	---	---	---	---	---	0.223	0.223
3.65	2,453	103.65	---	---	---	---	---	---	---	---	---	0.223	0.223
3.70	2,488	103.70	---	---	---	---	---	---	---	---	---	0.223	0.223
3.75	2,522	103.75	---	---	---	---	---	---	---	---	---	0.223	0.223
3.80	2,557	103.80	---	---	---	---	---	---	---	---	---	0.223	0.223
3.85	2,591	103.85	---	---	---	---	---	---	---	---	---	0.223	0.223
3.90	2,626	103.90	---	---	---	---	---	---	---	---	---	0.223	0.223
3.95	2,660	103.95	---	---	---	---	---	---	---	---	---	0.223	0.223
4.00	2,695	104.00	---	---	---	---	---	---	---	---	---	0.223	0.223
4.05	2,723	104.05	---	---	---	---	---	---	---	---	---	0.223	0.223
4.10	2,752	104.10	---	---	---	---	---	---	---	---	---	0.223	0.223
4.15	2,780	104.15	---	---	---	---	---	---	---	---	---	0.223	0.223
4.20	2,809	104.20	---	---	---	---	---	---	---	---	---	0.223	0.223
4.25	2,837	104.25	---	---	---	---	---	---	---	---	---	0.223	0.223
4.30	2,865	104.30	---	---	---	---	---	---	---	---	---	0.223	0.223
4.35	2,894	104.35	---	---	---	---	---	---	---	---	---	0.223	0.223
4.40	2,922	104.40	---	---	---	---	---	---	---	---	---	0.223	0.223
4.45	2,951	104.45	---	---	---	---	---	---	---	---	---	0.223	0.223
4.50	2,979	104.50	---	---	---	---	---	---	---	---	---	0.223	0.223
4.55	2,995	104.55	---	---	---	---	---	---	---	---	---	0.223	0.223
4.60	3,012	104.60	---	---	---	---	---	---	---	---	---	0.223	0.223
4.65	3,028	104.65	---	---	---	---	---	---	---	---	---	0.223	0.223
4.70	3,044	104.70	---	---	---	---	---	---	---	---	---	0.223	0.223
4.75	3,061	104.75	---	---	---	---	---	---	---	---	---	0.223	0.223
4.80	3,077	104.80	---	---	---	---	---	---	---	---	---	0.223	0.223
4.85	3,093	104.85	---	---	---	---	---	---	---	---	---	0.223	0.223
4.90	3,110	104.90	---	---	---	---	---	---	---	---	---	0.223	0.223
4.95	3,126	104.95	---	---	---	---	---	---	---	---	---	0.223	0.223
5.00	3,142	105.00	---	---	---	---	---	---	---	---	---	0.223	0.223

...End

